

Björn Matthias, ABB Corporate Research, 2015-09-28

The Role of Collision Experiments in Safety Standardization and in the Characterization of Collaborative Robots, Systems and Applications

Workshop IROS 2015 – Towards Standardized Experiments in Human-Robot Interactions



Collision Experiments for Safety and Characterization Overview

- What are we trying to achieve?
 - ➔ Objectives
- What do we have today?
 Overview of present criteria for comparison
- Who needs to do experiments?
 Players and responsibilities
- What do the experiments need to characterize?
 Physics of contact
- How should the experiments be done?
 Methods of measurement
- How can the results of the experiments be used?
 Quantities for Comparisons
- Summary and outlook



Collision Experiments for Safety and Characterization Objectives

- As stated clearly in workshop scope:
 - "... standardized assessment of robot products and applications in use in terms of safety, performance, user experience, and ergonomics."
- How easy or hard is this going to be?

		Safety	Performance	User Experience	Ergonomics
Principle	Objectivity, generalizable	0 → +	+	—	0
Method	Measurable, reproducible	+	+	0	+
Dissemination	Documented, available	0 → +	+	_	_



Collision Experiments for Safety and Characterization Overview of Present Criteria for Comparison

- Active standards
 - ISO 8373 "Manipulating industrial robots Vocabulary"
 - ISO 9283 "Manipulating industrial robots Performance criteria and related test methods"
 - ISO 9409 "Manipulating industrial robots Mechanical interfaces"
 - ISO 9787 "Robots and robotic devices Coordinate systems and motion nomenclatures"
 - ISO 9946 "Manipulating industrial robots Presentation of characteristics"
 - ISO 11593 "Manipulating industrial robots Automatic end-effector exchange systems Vocabulary and presentation of characteristics"
 - ISO 10218-1, -2 "Robots and robotic devices Safety requirements for industrial robots"
 - ISO 13482 "Robots and robotic devices Safety requirements for personal care robots"
 - ISO/TR 13309 "Manipulating industrial robots Informative guide on test equipment and metrology methods of operation for performance evaluation in accordance with ISO 9283
 - ISO 14539 "Manipulating industrial robots Object handling with grasp-type grippers Vocabulary and presentation of characteristics"
 - ISO/TS 15066 "Robots and robotic devices Safety requirements for industrial robots Collaborative operation"

(red = contains requirements needing experimental verification)



Collision Experiments for Safety and Characterization Overview of Present Criteria for Comparison

- Typical quantities in specifications and data sheets
 - By inspection testing not needed
 - Power source, electrical rating (ISO 8846)
 - Type (serial, parallel, Cartesian, ...), no. of joints, mounting orientation (ISO 9946)
 - Reach, dimensions of working space (ISO 9946)
 - Coordinate systems, base and flange (ISO 9946, ISO 9787)
 - Base mounting surface (ISO 9946), flange mounting surface (ISO 9946, ISO 9409)
 - Load (ISO 9946)
 - Environmental conditions, ingress protection (ISO 9946)
 - Testing needed for verification and comparison
 - Position accuracy, repeatability (ISO 9283)
 - Path accuracy, repeatability (ISO 9283)
 - Stopping behavior (ISO 10218-1)
 - Pick-and-place cycle 25 mm / 300 mm / 25 mm (adept)
 - Joint ranges, speeds, torques (often given optionally)
 - For power-and-force limited collaborative robots: quasi-static and transient contact situations (ISO/TS 15066)



Collision Experiments for Safety and Characterization Players and Responsibilities

Aspect	Robot Manufacturer	System Integrator	End-User
EU Machinery Directive or equiv.	 Incomplete machinery Technical construction file Declaration of incorporation No CE marking 	 Completed machinery Technical construction file Declaration of conformity CE marking 	 Operate only CE marked equipment
Risk Assessment	For robot manipulator	For complete applicationIntended useForeseeable misuse	(with integrator)
ISO 10218-1	 Basic safety requirements for industrial robots 	• N/A	• N/A
ISO 10218-2	• N/A	 Basic safety requirements for industrial robot systems 	• N/A
ISO/TS 15066	Specific requirements for collaborative robots	Specific requirements for collaborative applications	• N/A
Information for Use	 Safety configuration Exceptions to standards Exclusions (e.g. do not use this device for xxx) 	 Guidance for safe usage Intended use of equipment Exceptions, exclusions 	 Follow manufacturer and integrator documentation



Collision Experiments for Safety and Characterization Physics of Contact

- Types of collaborative operation
- Human-robot contact
 - Classification
 - Basic hazard types
- Models of contact events
 - Short duration (transient)
 - Two-body (in)elastic collision
 - Constrained / unconstrained
 - Sustained (quasi-static)
 - Forward kinematic transformation of joint torques
 - Constrained



Types of Collaborative Operation According to ISO 10218, ISO/TS 15066

ISO 10218-1, clause	Type of collaborative operation	Main means of risk reduction	
5.10.2	Safety-rated monitored stop (Example: manual loading-station)	No robot motion when operator is in collaborative work space	
5.10.3	Hand guiding (Example: operation as assist device)	Robot motion only through direct input of operator	
5.10.4	Speed and separation monitoring (Example: replenishing parts containers)	Robot motion only when separation distance above minimum separation distance	$v < v_{max}$ $d > d_{min}$
5.10.5	Power and force limiting by inherent design or control (Example: <i>ABB YuMi</i> ® collaborative assembly robot)	In contact events, robot can only impart limited static and dynamics forces	F < F _{max}



Speed and Separation Monitoring **Protective Separation Distance**



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Speed and Separation Monitoring Protective Separation Distance

$S_{protective}(t_0) = S_{human} + S_{reaction} + S_{stopping} + C$	$+ Z_S + Z_R$	
$S_{human} = \int_{t_0}^{t_0 + T_r + T_s} v_H(t) dt$	Here, $t_0 =$ "now" and $t =$ integration variable.	
$S = \int_{0}^{t_0+T_r} w(t) dt$		
$S_{reaction} - \int_{t_0} v_R(t) dt$	Condition for sufficient protection at	
$S_{stopping} = \int_{t_0+T_r}^{t_0+T_r+T_s} v_R(t) dt$	t_0 is $S_{measured}(t_0) \ge S_{protective}(t_0)$.	

Simple model assumptions (constant values) for $v_H(t)$ and for $v_R(t)$ in the reaction-phase of the robot motion can be made to give:

 $S_{human} = v_H(t_0) \cdot (T_r + T_s)$

 $S_{reaction} = v_R(t_0) \cdot T_r$

Values for the stopping distance $S_{stopping}$ should be obtained, as stated, from the data provided according to ISO 10218-1, Annex B.

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Human-Robot Contact Classification





Human-Robot Contact Basic Hazard Types

	Transient Contact	Quasi-Static Contact
Description	 Contact event is "short" (< 50 ms) Human body part can usually recoil 	 Contact duration is "extended" Human body part cannot recoil, is trapped
Limit Criteria	Peak forces, pressures, stressesEnergy transfer, power density	 Peak forces, pressures, stresses
Accessible in Design or Control	 Effective mass (robot pose, payload) Speed (relative) Contact area, duration 	 Force (joint torques, pose) Contact area, duration







Models of Contact Events Sustained Duration – Quasi-Static



- Compute forward kinematic transformation
- Apply to calculate contact forces and moments from joints torques



Models of Contact Events Short Duration – Transient



- Inelastic two-body contact
- Conservation of linear momentum
- Kinetic energy partly dissipated





Transient limit criteria related to robot design + control



• Force F [N]

• Pressure
$$p \left[\frac{N}{m^2} = \frac{J}{m^3}\right]$$

- Momentum transfer $q \left[\frac{kg \cdot m}{s}\right]$
- Energy transfer U [J]

• Power
$$P[W = \frac{J}{s}]$$

- Energy flux density $K\left[\frac{J}{m^2}\right]$
- Power flux density $S\left[\frac{W}{m^2}\right]$
- Contact area A [m²]



General approach – effective inelastic 2-body collision

- μ = reduced mass of 2-body system of robot and human body section
- v_{rel} = relative speed between robot and human body section
- C_R = coefficient of restitution
- k = effective spring constant of body area (here assumed constant)
- $x_1 = maximum$ compression of tissue in area of contact
- A_{avg} = average contact area during contact event
- F_{lim} , p_{lim} = force, pressure limit values for specific body region

Kinetic energy transfer:Worst-case assumption:Energy stored in "spring": $\Delta W = \frac{1}{2} \mu v_{rel}^2 (1 - C_R^2)$ $C_R = 0 \rightarrow \Delta W = \frac{1}{2} \mu v_{rel}^2$ $\Delta W = \frac{1}{2} k x_1^2 = \frac{F^2}{2k}$

Fully deposit kinetic energy into tissue as modeled by spring:

$$\frac{F^2}{2k} = \frac{1}{2} \mu v_{rel}^2 \quad \Rightarrow \quad v_{rel} = \frac{F}{\sqrt{\mu k}} = \frac{pA}{\sqrt{\mu k}} \quad \stackrel{F < F_{lim}}{\Rightarrow} \qquad v_{rel} < \frac{F_{lim}}{\sqrt{\mu k}} \approx \frac{p_{lim} A_{avg}}{\sqrt{\mu k}}$$
$$\mu = \left[\frac{1}{m_R} + \frac{1}{m_H}\right]^{-1}$$

Effective mass of robot (1) Proper formulation from complete equation of motion of robot

Equation of motion for stiff robot

 $M(q)\ddot{q} + C(q,\dot{q})\dot{q} + g(q) = \tau + \tau_c$

- $M \in \mathbb{R}^{n \times n}$: mass/inertia matrix
- $\boldsymbol{C} \in \mathbb{R}^{n \times n}$: centripetal and Coriolis matrix
- $\boldsymbol{g} \in \mathbb{R}^n$: gravity vector
- $oldsymbol{ au} \in \mathbb{R}^n$: joint motor torque vector

 $\boldsymbol{\tau_c} \in \mathbb{R}^n$: external contact torque vector

Effective mass in direction of unit vector
$$\boldsymbol{u}$$
:
 $m_u = [\boldsymbol{u}^T \boldsymbol{\Lambda}_t^{-1}(\boldsymbol{q}) \boldsymbol{u}]^{-1}$
where $\boldsymbol{\Lambda}(\boldsymbol{q}) = (\boldsymbol{J}(\boldsymbol{q}) (\boldsymbol{M}(\boldsymbol{q}))^{-1} \boldsymbol{J}^T(\boldsymbol{q}))^{-1}$

Kinetic energy $T = \frac{1}{2} \dot{\boldsymbol{q}}^T \boldsymbol{M}(\boldsymbol{q}) \dot{\boldsymbol{q}}$

Jacobian matrix J(q) such that $\dot{x} = J(q) \dot{q}$

Translational and rotational parts $J(q) = \begin{bmatrix} J_t(q) \\ J_r(q) \end{bmatrix}$

Effective mass of robot (2) Approximate formulation: Lumped parameter model



Example for stiff 3 DOF robot

- Effective moving mass at contact location (reflected inertia) m_R
- Speed of contact location \vec{v}_R
- Material properties of contact location
 - E.g. padding
- Compliance of kinematic chain
 - Can reduce effective mass

$$\vec{p}_R = \sum_i m_i \vec{v}_i \qquad m_R = \frac{\vec{p}_R \cdot \vec{v}_R}{v_R^2}$$



6 DOF articulated robot – Pose F (1) Straight from J2 to Flange, Rotation in J1

- For rotation about J1 and rigid joints J2, J3, J4, J5 and J6
 - Motion of J4, J6 not directly relevant, except if there is a heavy and asymmetric load on the flange
 - Speeds of COGs of links and load



•
$$v_{23} = \omega \frac{L_{23}}{2}$$

•
$$v_{34} = \omega \left(L_{23} + \frac{L_{34}}{2} \right)$$

• $v_{45} = \omega \left(L_{23} + L_{34} + \frac{L_{45}}{2} \right)$

•
$$v_{56} = \omega \left(L_{23} + L_{34} + L_{45} + \frac{L_{56}}{2} \right)$$

•
$$v_{6F} = \omega \left(L_{23} + L_{34} + L_{45} + L_{56} + \frac{L_{6F}}{2} \right)$$

•
$$v_L = \omega \left(L_{23} + L_{34} + L_{45} + L_{56} + L_{6F} \right)$$

Speeds at J3, F

$$M = M_{2F} = m_{23} + m_{34} + m_{45} + m_{56} + m_{6F} \quad \cdot v_3 = \omega L_{23}$$
$$L_{2F} = L_{23} + L_{34} + L_{45} + L_{56} + L_{6F} \quad \cdot v_F = \omega (L_{23} + L_{34} + L_{45} + L_{56} + L_{6F})$$

6 DOF articulated robot – Pose F (2) Straight from J2 to Flange, Rotation in J1

- For rotation about J1 and rigid joints J2, J3, J4, J5 and J6
 - Motion of J4, J6 not directly relevant, except if there is a heavy and asymmetric load on the flange
 - Momentum of COGs of links and load

•
$$p_{23} = m_{23}v_{23} = \omega m_{23} \frac{L_{23}}{2}$$

•
$$p_{34} = m_{34}v_{34} = \omega m_{34} \left(L_{23} + \frac{L_{34}}{2} \right)$$

•
$$p_{45} = m_{45}v_{45} = \omega m_{45} \left(L_{23} + L_{34} + \frac{L_{45}}{2} \right)$$

•
$$p_{56} = m_{56}v_{56} = \omega m_{56} \left(L_{23} + L_{34} + L_{45} + \frac{L_{56}}{2} \right)$$

•
$$p_{6F} = m_{6F}v_{6F} = \omega m_{6F} \left(L_{23} + L_{34} + L_{45} + L_{56} + \frac{L_{6F}}{2} \right)$$

•
$$p_L = m_L v_F = \omega m_L (L_{23} + L_{34} + L_{45} + L_{56} + L_{6F})$$

- Effective mass for contact at elbow (J3)

•
$$m_{eff}(J3) = \frac{p_{23} + p_{34} + p_{45} + p_{56} + p_{6F} + p_L}{v_3} = \frac{L_{2F}}{L_{23}} \left[\frac{M_{2F}}{2} + m_L \right]$$

Effective mass for contact at flange (F)

$$M = M_{2F} = m_{23} + m_{34} + m_{45} + m_{56} + m_{6F} \quad \cdot \quad m_{eff}(F) = \frac{p_{23} + p_{34} + p_{45} + p_{56} + p_{6F} + p_L}{v_F} = \frac{M_{2F}}{2} + m_L$$

$$L_{2F} = L_{23} + L_{34} + L_{45} + L_{56} + L_{6F}$$





ISO/TS 15066 – Present Status Body Model



Figure A.1 — Body Model

Table A.1 — Body Model Descriptions

			Front/
Body Region	Specific Body Area		Rear
Skull and forehead	1	Middle of forehead	Front
	2	Temple	Front
Face	3	Masticatory muscle	Front
Neck	4	Neck muscle	Rear
	5	Seventh neck vertebra	Rear
Back and shoulders	6	Shoulder joint	Front
	7	Fifth lumbar vertebra	Rear
Chest	8	Sternum	Front
	9	Pectoral muscle	Front
Abdomen	10	Abdominal muscle	Front
Pelvis	11	Pelvic bone	Front
Upper arms and elbow	12	Deltoid muscle	Rear
joints			
	13	Humerus	Rear
	16	Arm nerve	Front
Lower arms and wrist joints	14	Radial bone	Rear
	15	Forearm muscle	Rear
Hands and fingers	17	Forefinger pad D	Front
	18	Forefinger pad ND	Front
	19	Forefinger end joint D	Rear
	20	Forefinger end joint ND	Rear
	21	Thenar eminence	Front
	22	Palm D	Front
	23	Palm ND	Front
	24	Back of the hand D	Rear
	25	Back of the hand ND	Rear
Thighs and knees	26	Thigh muscle	Front
	27	Kneecap	Front
Lower legs	28	Middle of shin	Front
	29	Calf muscle	Rear



Collision Experiments for Safety and Characterization Methods of Measurement



- Visco-elastic properties of body area in spring-damper element
- Mass m chosen to represent effective mass of body area
- Measure over time
 - Contact area, pressure distribution
 - Forces, torques, displacement



Experimental Characterization of Collaborative Robot Collisions Experimental Setups















Experimental Characterization of Collaborative Robot Collisions Experimental Setup



rosetta

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Experimental Characterization of Collaborative Robot Collisions Experimental Setups







Collision Experiments for Safety and Characterization Quantities for Comparisons

- Quasi-static contact events
 - Characterized by forces and pressures, contact area
 - Controlled by joint torque limitation (safety-related control function or electro-mechanical design)
- Transient contact events
 - Characterized by energy transfer, contact area, duration (power flux density)
 - Controlled by limiting robot speed



Collision Experiments for Safety and Characterization Summary and Outlook

- Collision experiments are necessary to establish suitability of robots for collaborative operation according to powerand-force-limiting
- Collision data can be used to verify and validate simulations of contact events for a given robot type
- Experimental set ups and practical challenges
- Comparison of contact event characteristics is possible for given robot motion or pose
- Future or deployment of collaborative applications
 - → use validated robot with experimental collision data and simulation model
 - → determine limit parameters (torques, forces, speeds) of robot motion from simulation of target application



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